

# Micropower, Rail to Rail Input Current Sense Amplifier with Voltage Output

### ISL28006

The ISL28006 is a micropower, uni-directional high-side and low-side current sense amplifier featuring a proprietary rail-to-rail input current sensing amplifier. The ISL28006 is ideal for high-side current sense applications where the sense voltage is usually much higher than the amplifier supply voltage. The device can be used to sense voltages as high as 28V when operating from a supply voltage as low as 2.7V. The micropower ISL28006 consumes only 50µA of supply current when operating from a 2.7V to 28V supply.

The ISL28006 features a common-mode input voltage range from OV to 28V. The proprietary architecture extends the input voltage sensing range down to OV, making it an excellent choice for low-side ground sensing applications. The benefit of this architecture is that a high degree of total output accuracy is maintained over the entire OV to 28V common mode input voltage range.

The ISL28006 is available in fixed (100V/V, 50V/V, 20V/V and Adjustable) gains in the space saving 5 Ld SOT-23 package and the 6 Ld SOT-23 package for the adjustable gain part. The parts operate over the extended temperature range from -40  $^{\circ}$ C to +125  $^{\circ}$ C.

### **Features**

•	Low Power Consumption
•	Supply Range
•	Wide Common Mode Input
•	Gain Versions
	- ISL28006-100
	- ISL28006-50 50V/V
	- ISL28006-20 20V/V
	- ISL28006-ADJ ADJ (Min Gain = 20V/V)
•	Operating Temperature Range 40 $^{\circ}$ C to +125 $^{\circ}$ C
•	Packages 5 Ld SOT-23, 6 Ld SOT-23

## **Applications**

- · Power Management/Monitors
- · Power Distribution and Safety
- DC/DC, AC/DC Converters
- · Battery Management/Charging
- Automotive Power Distribution

## **Related Literature**

• See AN1532 for "ISL28006 Evaluation Board User's Guide"

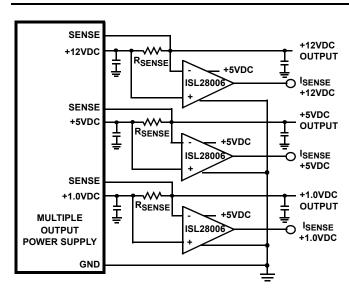


FIGURE 1. TYPICAL APPLICATION

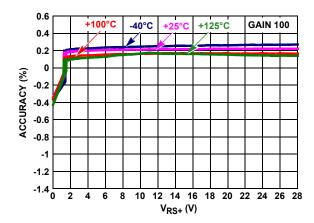
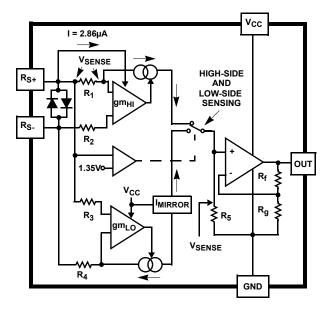
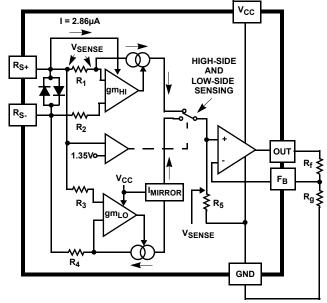


FIGURE 2. GAIN ACCURACY vs V<sub>RS+</sub> = 0V TO 28V

## **Block Diagram**

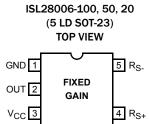


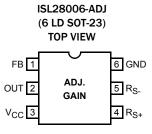


**FIXED GAIN PARTS** 

ADJUSTABLE GAIN PART

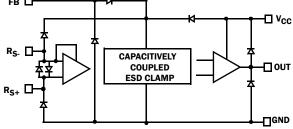
## **Pin Configurations**





## **Pin Descriptions**

ISL28006-100, 50, 20	ISL28006-ADJ		D.F.O.D.IDTION
(5 LD SOT-23)	(6 LD SOT-23)	PIN NAME	DESCRIPTION
1	6	GND	Power Ground
	1	FB	Input Pin for External Resistors
2	2	OUT	Amplifier Output
3	3	v <sub>cc</sub>	Positive Power Supply
4	4	R <sub>S+</sub>	Sense Voltage Non-inverting Input
5	5	R <sub>S-</sub>	Sense Voltage Inverting Input
	FB □	N	



## **Ordering Information**

PART NUMBER (Notes 1, 2, 3)	GAIN	PART MARKING	PACKAGE Tape & Reel (Pb-Free)	PKG. DWG.#	
ISL28006FH100Z-T7	100V/V	BDJA (Note 4)	5 Ld SOT-23	P5.064A	
ISL28006FH100Z-T7A	100V/V	BDJA (Note 4)	5 Ld SOT-23	P5.064A	
ISL28006FH50Z-T7	50V/V	BDHA (Note 4)	5 Ld SOT-23	P5.064A	
ISL28006FH50Z-T7A	50V/V	BDHA (Note 4)	5 Ld SOT-23	P5.064A	
ISL28006FH20Z-T7	20V/V	BDGA (Note 4)	5 Ld SOT-23	P5.064A	
ISL28006FH20Z-T7A	20V/V	BDGA (Note 4)	5 Ld SOT-23	P5.064A	
ISL28006FHADJZ-T7	ADJ	BDFA (Note 4)	6 Ld SOT-23	P6.064	
ISL28006FHADJZ-T7A	ADJ	BDFA (Note 4)	6 Ld SOT-23	P6.064	
ISL28006FH-100EVAL1Z	100V/V Evaluation	Board	1	1	
ISL28006FH-50EVAL1Z	50V/V Evaluation B	Board			
ISL28006FH-20EVAL1Z	20V/V Evaluation Board				
ISL28006FH-ADJEVAL1Z	Adjustable Evaluation Board				

#### NOTES:

- 1. Please refer to  $\underline{\mathsf{TB347}}$  for details on reel specifications.
- 2. These Intersil Pb-free plastic packaged products employ special Pb-free material sets, molding compounds/die attach materials, and 100% matte tin plate plus anneal (e3 termination finish, which is RoHS compliant and compatible with both SnPb and Pb-free soldering operations). Intersil Pb-free products are MSL classified at Pb-free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020.
- 3. For Moisture Sensitivity Level (MSL), please see device information page for ISL28006. For more information on MSL please see techbrief TB363.
- 4. The part marking is located on the bottom of the part.

### **Absolute Maximum Ratings**

Max Supply Voltage
Max Differential Input Current
Max Differential Input Voltage±0.5V
Max Input Voltage (R <sub>S+</sub> , R <sub>S-</sub> , FB) GND - 0.5V to 30V
Max Input Current for Input Voltage <gnd -="" 0.5v="" td="" ±20ma<=""></gnd>
Output Short-Circuit Duration Indefinite
Di-Electrically Isolated PR40 Process Latch-up free
ESD Rating
Human Body Model (Tested per JESD22-A114F) 4kV
Machine Model (Tested per EIA/JESD22-A115-A)200V
Charged Device Model (Tested per JESD22-C101D)

#### **Thermal Information**

Thermal Resistance (Typical)	$\theta_{JA}$ (°C/W)	$\theta_{JC}$ (°C/W)
5 Ld SOT-23 (Notes 5, 6)	190	90
6 Ld SOT-23 (Notes 5, 6)	180	90
Maximum Storage Temperature Range	(	65°C to +150°C
Maximum Junction Temperature (T <sub>JMAX</sub> )		+150°C
Pb-Free Reflow Profile		. see link below
http://www.intersil.com/pbfree/Pb-FreeRe	eflow.asp	

#### **Recommended Operating Conditions**

Ambient Temperature Range (T<sub>A</sub>) .....-40 °C to +125 °C

CAUTION: Do not operate at or near the maximum ratings listed for extended periods of time. Exposure to such conditions may adversely impact product reliability and result in failures not covered by warranty.

#### NOTES

- 5.  $\theta_{JA}$  is measured with the component mounted on a high effective thermal conductivity test board in free air. See Tech Brief TB379 for details.
- 6. For  $\theta_{\mbox{\scriptsize JC}}\!,$  the "case temp" location is taken at the package top center.

**Electrical Specifications**  $V_{CC} = 12V$ ,  $V_{RS+} = 0V$  to 28V,  $V_{SENSE} = 0V$ ,  $R_{LOAD} = 1M\Omega$ ,  $T_A = +25\,^{\circ}C$  unless otherwise specified. Boldface limits apply over the operating temperature range,  $-40\,^{\circ}C$  to  $+125\,^{\circ}C$ . Temperature data established by characterization.

PARAMETER	DESCRIPTION	CONDITIONS	MIN (Note 7)	TYP	MAX (Note 7)	UNIT
v <sub>os</sub>	Gain = 100	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>SENSE</sub> = 20mV to 100mV	-250	60	250	μV
(Input Offset Voltage)	(Notes 8, 9)		-300		300	μV
,		$V_{CC} = 12V$ , $V_{RS} + = 0.2V$ , $V_{SENSE} = 20mV$ to 100mV	-2.5	-1.2	2.5	m۷
			-2.8		2.8	m۷
	Gain = 50, Gain = 20	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>SENSE</sub> = 20mV to 100mV	-300	60	300	μV
	(Notes 8, 9)		-450		450	μV
		$V_{CC} = 12V$ , $V_{RS} + = 0.2V$ , $V_{SENSE} = 20mV$ to 100mV	-2.8	-1.2	2.8	m۷
			-3.2		3.2	m۷
	Adjustable, Gain = 21	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>SENSE</sub> = 20mV to 100mV	-300	60	300	μV
	$R_f = 100k\Omega$ , $R_g = 5k\Omega$ (Notes 8, 9)		-450		450	μV
		V <sub>CC</sub> = 12V, V <sub>RS</sub> + = 0.2V, V <sub>SENSE</sub> = 20mV to 100mV	-3.1	-1.2	3.1	m۷
			-3.4		3.4	m۷
I <sub>RS</sub> +, I <sub>RS</sub> -	Leakage Current	V <sub>CC</sub> = 0V, V <sub>RS+</sub> = 28V		0.041	1.2	μΑ
					1.5	μΑ
I <sub>RS</sub> +		$V_{RS}$ + = 2V, $V_{SENSE}$ = 5mV		4.7	6	μΑ
(+ Input Bias Current)					7	μΑ
,		$V_{RS}$ + = 0V, $V_{SENSE}$ = 5mV	-500	-432		nA
			-600			nA
	Gain = 50, Gain = 20 $ADJ \ Gain = 101$ $R_f = 100k\Omega, \ R_g = 1k\Omega$	$V_{RS}$ + = 2V, $V_{SENSE}$ = 5mV		4.7	6	μΑ
					8	μΑ
		$V_{RS}$ + = 0V, $V_{SENSE}$ = 5mV	-700	-432		nA
			-840			nA
		V <sub>RS</sub> + = 2V, V <sub>SENSE</sub> = 5mV		4.7	6	μΑ
					7	μΑ
		V <sub>RS</sub> + = 0V, V <sub>SENSE</sub> = 5mV	-500	-432		nA
			-600			nA

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**Electrical Specifications**  $V_{CC} = 12V$ ,  $V_{RS+} = 0V$  to 28V,  $V_{SENSE} = 0V$ ,  $R_{LOAD} = 1M\Omega$ ,  $T_A = +25\,^{\circ}C$  unless otherwise specified. Boldface limits apply over the operating temperature range, -40 °C to +125 °C. Temperature data established by characterization. (Continued)

PARAMETER	DESCRIPTION	CONDITIONS	MIN (Note 7)	TYP	MAX (Note 7)	UNIT
I <sub>RS</sub> -	G = 100, 50, 20, ADJ	$V_{RS}$ + = 2V, $V_{SENSE}$ = 5mV		5	50	nA
(- Input Bias Current)					75	nA
ourront,		$V_{RS}$ + = 0V, $V_{SENSE}$ = 5mV	-125	-45		nA
			-130			nA
CMRR	Common Mode Rejection Ratio	V <sub>RS</sub> + = 2V to 28V	105	115		dB
PSRR	Power Supply Rejection Ratio	V <sub>CC</sub> = 2.7V to 28V, V <sub>RS</sub> + = 2V	90	105		dB
V <sub>FS</sub>	Full-scale Sense Voltage	V <sub>CC</sub> = 28V, V <sub>RS</sub> + = 0.2V, 12V	200			mV
G	(Note 8)	ISL28006-100		100		V/V
(Gain)		ISL28006-50		50		V/V
		ISL28006-20		20		V/V
		ISL28006-ADJ	20			V/V
G <sub>A</sub>	Gain = 100	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>SENSE</sub> = 20mV to 100mV	-0.2		0.7	%
(Gain Accuracy)	(Note 10)		-1		1	%
		V <sub>CC</sub> = 12V, V <sub>RS</sub> + = 0.1V, V <sub>SENSE</sub> = 20mV to 100mV		-0.25		%
	Gain = 50, Gain = 20	$V_{CC} = V_{RS} + = 12V, V_{SENSE} = 20mV \text{ to } 100mV$	-0.35		0.7	%
	(Note 10)		-1		1	%
		$V_{CC} = 12V$ , $V_{RS} + = 0.1V$ , $V_{SENSE} = 20$ mV to 100mV	-2.2	-0.33	2.2	%
			-2.3		2.3	%
	ADJ Gain = 21 $R_f = 100k\Omega$ , $R_g = 5k\Omega$ (Note 10)	$V_{CC} = V_{RS} + = 12V$ , $V_{SENSE} = 20mV$ to 100mV $V_{CC} = 12V$ , $V_{RS} + = 0.1V$ , $V_{SENSE} = 20mV$ to 100mV	-0.65		1	%
			-1		1.05	%
	(1.010 = 0)		-2.2	-0.33	2.2	%
			-2.3		2.3	
V <sub>OA</sub>	Gain = 100 (Note 11)	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>SENSE</sub> = 100mV	-0.7		0.7	%
(Total Output Accuracy)			-0.9		0.9	%
,,,,,,		V <sub>CC</sub> = 12V, V <sub>RS</sub> + = 0.1V, V <sub>SENSE</sub> = 100mV		-1.25		%
	Gain = 50, Gain = 20 (Note 11)	$V_{CC} = V_{RS} + = 12V$ , $V_{SENSE} = 100$ mV	-0.7		0.7	%
			-0.9		0.9	%
		V <sub>CC</sub> = 12V, V <sub>RS</sub> + = 0.1V, V <sub>SENSE</sub> = 100mV	-4.7	-1.41	1.8	%
			-5.2		2.3	%
	ADJ Gain = 21 $R_f = 100k\Omega$ , $R_g = 5k\Omega$ (Note 11)	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>SENSE</sub> = 100mV	-0.7		1.05	%
			-0.9		1.2	%
	,	$V_{CC} = 12V, V_{RS} + = 0.1V, V_{SENSE} = 100mV$	-4.7	-1.41	1.8	%
			-5.2		2.3	%
V <sub>OH</sub>	Output Voltage Swing, High V <sub>CC</sub> - V <sub>OUT</sub>	$I_0 = -500 \mu A$ , $V_{CC} = 2.7 V$ , $V_{SENSE} = 100 mV$ , $V_{RS} + = 2 V$		39	50	mV
V <sub>OL</sub>	Output Voltage Swing, Low V <sub>OUT</sub>	$I_0 = 500 \mu A$ , $V_{CC} = 2.7 V$ , $V_{SENSE} = 0 V$ , $V_{RS} + = 2 V$		30	50	mV
R <sub>OUT</sub>	Output Resistance	$V_{CC} = V_{RS} + = 12V$ , $V_{SENSE} = 100$ mV, $I_{OUT} = 10 \mu A$ to 1mA		6.5		Ω
I <sub>SC+</sub>	Short Circuit Sourcing Current	$V_{CC} = V_{RS} + = 5V$ , $R_L = 10\Omega$		4.8		mA
I <sub>SC-</sub>	Short Circuit Sinking Current	$V_{CC} = V_{RS} + = 5V$ , $R_L = 10\Omega$		8.7		mA

### **ISL28006**

**Electrical Specifications**  $V_{CC} = 12V$ ,  $V_{RS+} = 0V$  to 28V,  $V_{SENSE} = 0V$ ,  $R_{LOAD} = 1M\Omega$ ,  $T_A = +25^{\circ}C$  unless otherwise specified. Boldface limits apply over the operating temperature range,  $-40^{\circ}C$  to  $+125^{\circ}C$ . Temperature data established by characterization. (Continued)

PARAMETER	DESCRIPTION	CONDITIONS		TYP	MAX (Note 7)	UNIT
Icc	Gain = 100	V <sub>RS</sub> + > 2V, V <sub>SENSE</sub> = 5mV		50	59	μΑ
					62	μΑ
	Gain = 50, 20,	V <sub>RS</sub> + > 2V, V <sub>SENSE</sub> = 5mV		50	62	μΑ
					63	μΑ
	ADJ Gain = 21	V <sub>RS</sub> + > 2V, V <sub>SENSE</sub> = 5mV		50	62	μΑ
	$R_f = 100k\Omega$ , $R_g = 5k\Omega$				63	μΑ
V <sub>CC</sub>	Supply Voltage	Guaranteed by PSRR	2.7		28	V
Slew Rate	Gain = 100	Pulse on R <sub>S+</sub> pin, V <sub>OUT</sub> = 8V <sub>P-P</sub> (Figure 75)	0.58	0.76		V/µs
	Gain = 50	Pulse on R <sub>S+</sub> pin, V <sub>OUT</sub> = 8V <sub>P-P</sub> (Figure 75)	0.58	0.67		V/µs
	Gain = 20	Pulse on R <sub>S+</sub> pin, V <sub>OUT</sub> = 3.5V <sub>P-P</sub> (Figure 75)	0.50	0.67		V/µs
	ADJ Gain = 21 $R_f = 100k\Omega$ , $R_g = 5k\Omega$	Pulse on R <sub>S+</sub> pin, V <sub>OUT</sub> = 3.5V <sub>P-P</sub> (Figure 75)	0.50	0.67		V/µs
BW <sub>-3dB</sub>	Gain = 100	V <sub>RS</sub> + = 12V, 0.1V, V <sub>SENSE</sub> = 100mV		110		kHz
	Gain = 50	V <sub>RS</sub> + = 12V, 0.1V, V <sub>SENSE</sub> = 100mV		160		kHz
	Gain = 20	V <sub>RS</sub> + = 12V, 0.1V, V <sub>SENSE</sub> = 100mV		180		kHz
	ADJ, Gain = 101 (Figure 65)	$V_{RS}$ + = 12V, 0.1V, $V_{SENSE}$ = 100mV, $R_f$ = 100k $\Omega$ , $R_g$ = 1k $\Omega$		40		kHz
	ADJ, Gain = 51 (Figure 65)	$V_{RS}$ + = 12V, $V_{SENSE}$ = 100mV, $R_f$ = 100k $\Omega$ , $R_g$ = 2k $\Omega$		78		kHz
		$V_{RS}$ + = 0.1V, $V_{SENSE}$ = 100mV, $R_f$ = 100k $\Omega$ , $R_g$ = 2k $\Omega$		122		kHz
	ADJ, Gain = 21 (Figure 65)	$V_{RS}$ + = 12V, $V_{SENSE}$ = 100mV, $R_f$ = 100k $\Omega$ , $R_g$ = 5k $\Omega$		131		kHz
		$V_{RS}$ + = 0.1V, $V_{SENSE}$ = 100mV, $R_f$ = 100k $\Omega$ , $R_g$ = 5k $\Omega$		237		kHz
t <sub>S</sub>	Output Settling Time to 1% of Final	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>OUT</sub> = 10V step, V <sub>SENSE</sub> > 7mV		15		μs
	Value	V <sub>CC</sub> = V <sub>RS</sub> + = 0.2V, V <sub>OUT</sub> = 10V step, V <sub>SENSE</sub> > 7mV		20		μs
	Capacitive-Load Stability	No sustained oscillations		300		pF
t <sub>S Power-up</sub>	Power-Up Time to 1% of Final Value	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>SENSE</sub> = 100mV		15		μs
		V <sub>CC</sub> = 12V, V <sub>RS</sub> + = 0.2V, V <sub>SENSE</sub> = 100mV		50		μs
	Saturation Recovery Time	V <sub>CC</sub> = V <sub>RS</sub> + = 12V, V <sub>SENSE</sub> = 100mV, overdrive		10		μs

#### NOTES:

7. Compliance to datasheet limits is assured by one or more methods: production test, characterization and/or design.

#### 8. DEFINITION OF TERMS:

- V<sub>SENSE</sub>A = V<sub>SENSE</sub> @ 100mV
- V<sub>SENSE</sub>B = V<sub>SENSE</sub> @ 20mV
- V<sub>OUT</sub>A = V<sub>OUT</sub> @ V<sub>SENSE</sub>A = 100mV
- V<sub>OUT</sub>B = V<sub>OUT</sub> @ V<sub>SENSE</sub>B = 20mV

$$\bullet \ \mbox{G = GAIN} \ = \left( \frac{\mbox{$V_{OUT}$A} - \mbox{$V_{OUT}$B}}{\mbox{$V_{SENSE}$B}} \right) \label{eq:gain}$$

9.  $V_{OS}$  is extrapolated from the gain measurement.  $V_{OS} = V_{SENSE}A - \frac{V_{OUT}A}{G}$ 

$$\textbf{10. \% Gain Accuracy} = \textbf{G}_{\textbf{A}} = \left(\frac{\textbf{G}_{\textbf{MEASURED}} - \textbf{G}_{\textbf{EXPECTED}}}{\textbf{G}_{\textbf{EXPECTED}}}\right) \times \textbf{100}$$

 $\textbf{11. Output Accuracy \% VOA} = \left(\frac{\text{VOUT}_{\text{MEASURED}} - \text{VOUT}_{\text{EXPECTED}}}{\text{VOUT}_{\text{EXPECTED}}}\right) \times \textbf{100, where V}_{\text{OUT}} = \textbf{V}_{\text{SENSE}} \, \textbf{X GAIN and V}_{\text{SENSE}} = \textbf{100mV}$ 

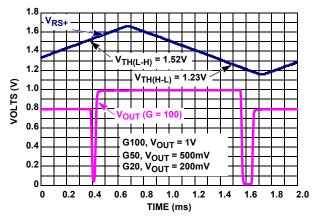


FIGURE 3. HIGH-SIDE and LOW-SIDE THRESHOLD VOLTAGE  $V_{RS+(L-H)} \ and \ V_{RS+(H-L)}, \ V_{SENSE} = \textbf{10mV}$ 

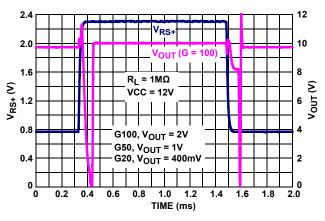


FIGURE 4. V<sub>OUT</sub> vs V<sub>RS+</sub>, V<sub>SENSE</sub> = 20mV TRANSIENT RESPONSE

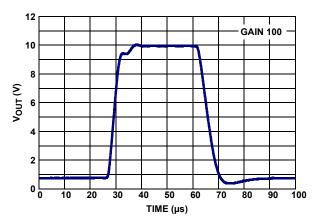


FIGURE 5. LARGE SIGNAL TRANSIENT RESPONSE  $V_{RS+} = 0.2V$ ,  $V_{SENSE} = 100 \text{mV}$ 

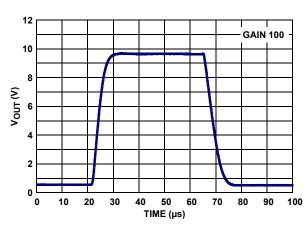


FIGURE 6. LARGE SIGNAL TRANSIENT RESPONSE  $V_{RS+} = 12V$ ,  $V_{SENSE} = 100 \text{mV}$ 

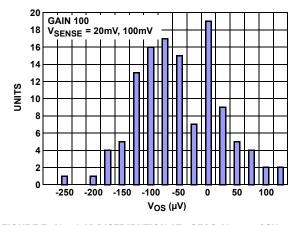


FIGURE 7.  $V_{OS}(\mu V)$  DISTRIBUTION AT +25 ° C,  $V_{RS+}$  = 12V, QUANTITY: 100

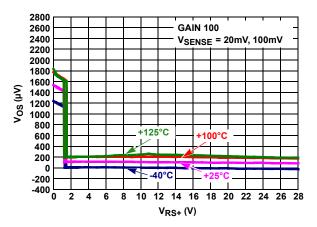


FIGURE 8. VOS VS VRS+

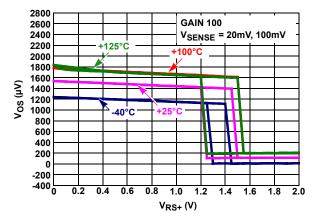


FIGURE 9. VOS VS VRS+

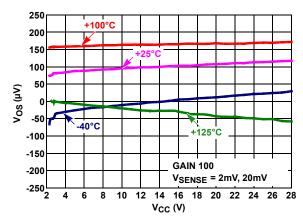


FIGURE 10. VOS vs VCC, VRS+= 12V

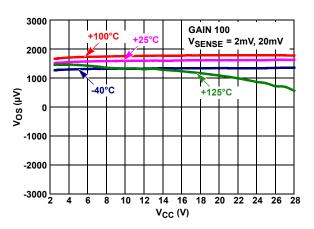


FIGURE 11.  $V_{OS}$  vs  $V_{CC}$ ,  $V_{RS+} = 0.1V$ 

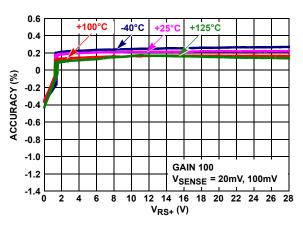


FIGURE 12. GAIN ACCURACY vs  $V_{RS+} = 0V TO 28V$ 

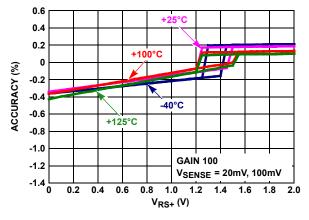


FIGURE 13. GAIN ACCURACY vs V<sub>RS+</sub> = 0V TO 2V

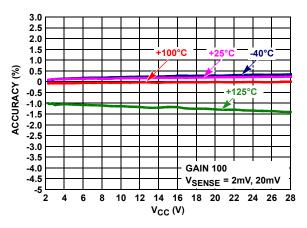


FIGURE 14. GAIN ACCURACY vs  $V_{CC}$ ,  $V_{RS+} = 12V$ 

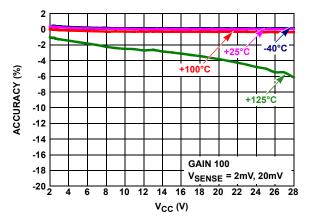


FIGURE 15. GAIN ACCURACY vs  $V_{CC}$ ,  $V_{RS+} = 0.1V$ 

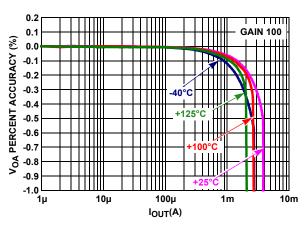


FIGURE 16. NORMALIZED  $V_{OA}$  vs  $I_{OUT}$ 

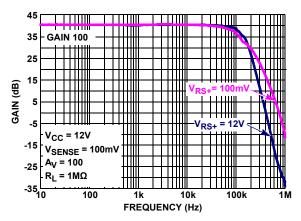


FIGURE 17. GAIN vs FREQUENCY  $V_{RS+} = 100 \text{mV}/12 \text{V},$   $V_{SENSE} = 100 \text{mV}, V_{OUT} = 50 \text{mV}_{P-P}$ 

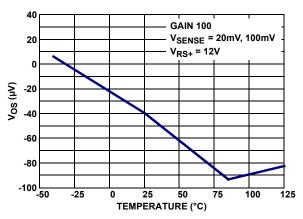


FIGURE 18.  $V_{OS}$  ( $\mu V$ ) vs TEMPERATURE

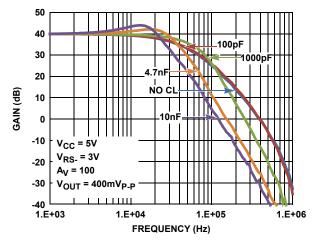


FIGURE 19. CAPACITIVE LOAD DRIVE GAIN vs FREQUENCY

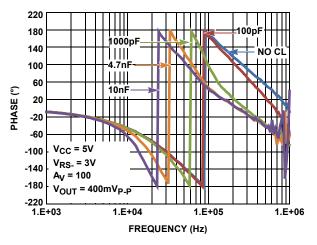


FIGURE 20. CAPACITIVE LOAD DRIVE PHASE vs FREQUENCY

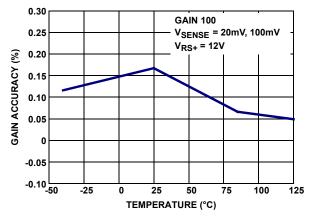


FIGURE 21. GAIN ACCURACY (%) vs TEMPERATURE

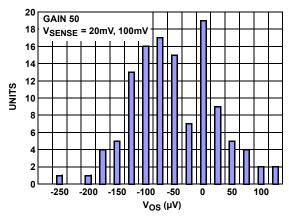


FIGURE 23.  $V_{OS}$  (µV) DISTRIBUTION AT +25 °C,  $V_{RS+}$  = 12V, QUANTITY: 100

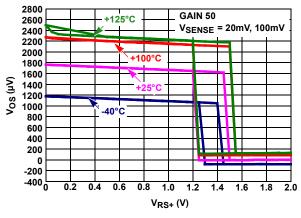


FIGURE 25. VOS VS VRS+

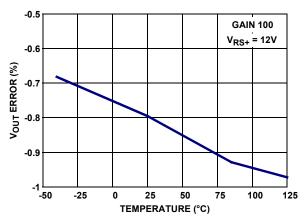


FIGURE 22. V<sub>OUT</sub> ERROR (%) vs TEMPERATURE

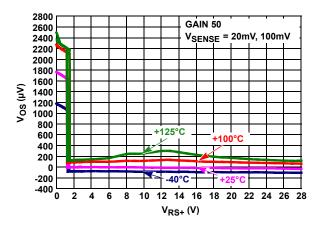


FIGURE 24. V<sub>OS</sub> vs V<sub>RS+</sub>

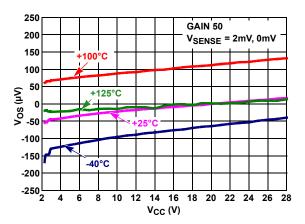


FIGURE 26.  $V_{OS}$  vs  $V_{CC}$ ,  $V_{RS+} = 12V$ 

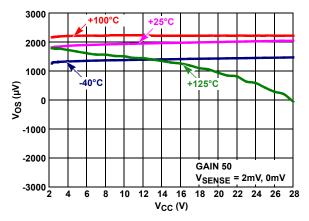


FIGURE 27.  $V_{OS}$  vs  $V_{CC}$ ,  $V_{RS+} = V_{RS+} = 0.1V$ 

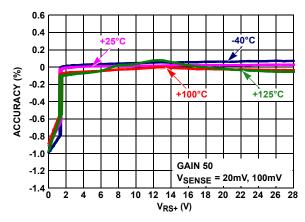


FIGURE 28. GAIN ACCURACY vs V<sub>RS+</sub> = 0V TO 28V

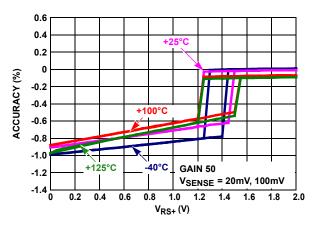


FIGURE 29. GAIN ACCURACY vs V<sub>RS+</sub> = 0V TO 2V

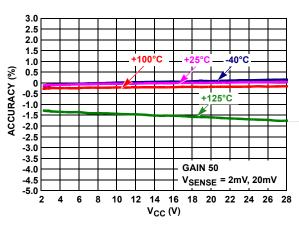


FIGURE 30. GAIN ACCURACY vs  $V_{CC}$ , HIGH-SIDE

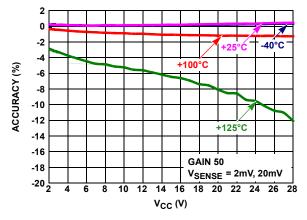


FIGURE 31. GAIN ACCURACY vs  $V_{CC}$ , LOW-SIDE

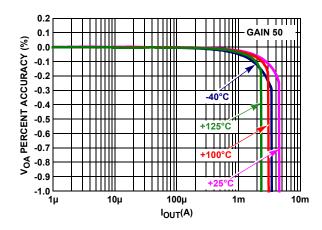


FIGURE 32. NORMALIZED  $V_{OA}$  vs  $I_{OUT}$ 

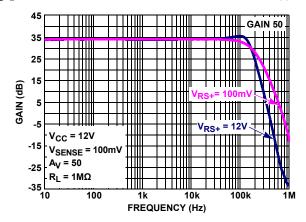


FIGURE 33. GAIN vs FREQUENCY  $V_{RS+} = 100 \text{mV}/12 \text{V}$ ,  $V_{SENSE} = 100 \text{mV}$ ,  $V_{OUT} = 50 \text{mV}_{P-P}$ 

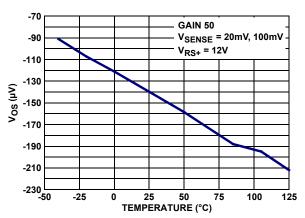


FIGURE 34.  $V_{OS}$  ( $\mu V$ ) vs TEMPERATURE

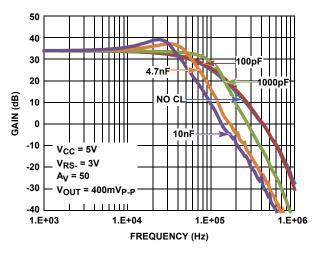


FIGURE 35. CAPACITIVE LOAD DRIVE GAIN vs FREQUENCY

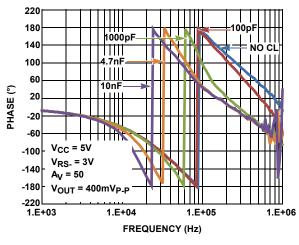


FIGURE 36. CAPACITIVE LOAD DRIVE PHASE vs FREQUENCY

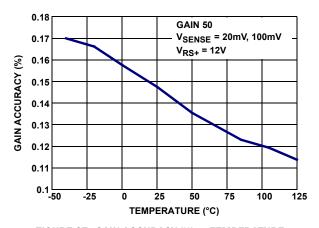


FIGURE 37. GAIN ACCURACY (%) vs TEMPERATURE

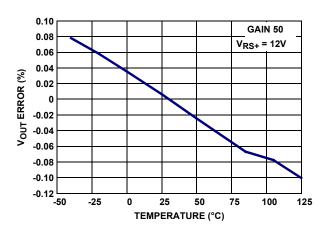


FIGURE 38. V<sub>OUT</sub> ERROR (%) vs TEMPERATURE

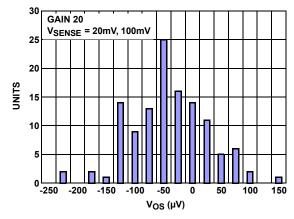


FIGURE 39.  $V_{OS}$  (µV) DISTRIBUTION AT +25 °C,  $V_{RS+}$  = 12V, QUANTITY: 100

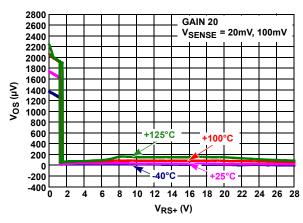


FIGURE 40.  $V_{OS}$  vs  $V_{RS+}$ 

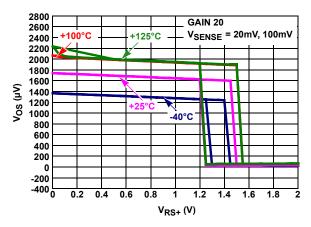


FIGURE 41. V<sub>OS</sub> vs V<sub>RS+</sub>

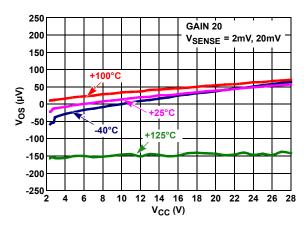


FIGURE 42. V<sub>OS</sub> vs V<sub>CC</sub>, V<sub>RS+</sub> = 12V

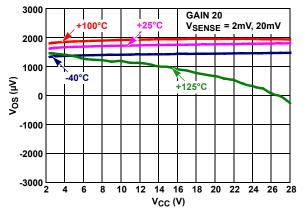


FIGURE 43.  $V_{OS}$  vs  $V_{CC}$ ,  $V_{RS+} = 0.1V$ 

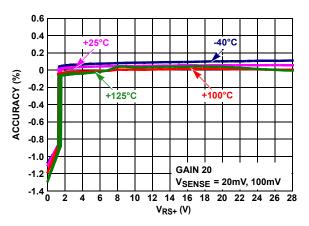


FIGURE 44. GAIN ACCURACY vs V<sub>RS+</sub> = 0V TO 28V

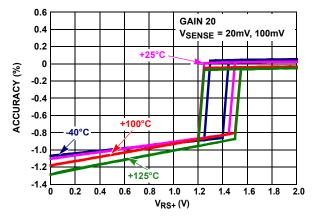


FIGURE 45. GAIN ACCURACY vs V<sub>RS+</sub> = 0V TO 2V

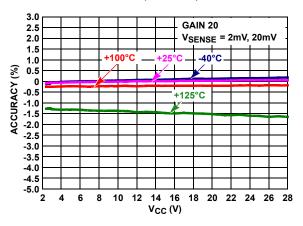


FIGURE 46. GAIN ACCURACY vs V<sub>CC</sub>, HIGH-SIDE

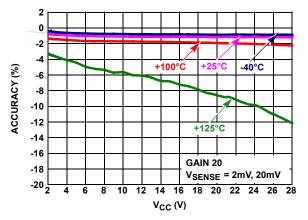


FIGURE 47. GAIN ACCURACY vs  $V_{CC}$ , LOW-SIDE

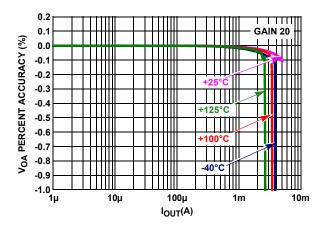


FIGURE 48. NORMALIZED V<sub>OA</sub> vs I<sub>OUT</sub>

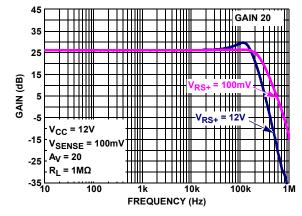


FIGURE 49. GAIN vs FREQUENCY  $V_{RS+}$  = 100mV/12V,  $V_{SENSE}$  = 100mV,  $V_{OUT}$  = 50mV<sub>P-P</sub>

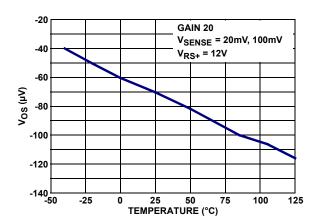


FIGURE 50.  $V_{OS}$  ( $\mu V$ ) vs TEMPERATURE

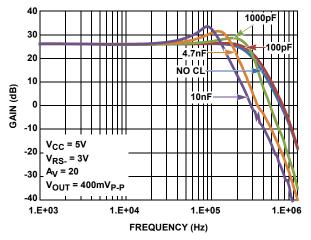


FIGURE 51. CAPACITIVE LOAD DRIVE GAIN VS FREQUENCY

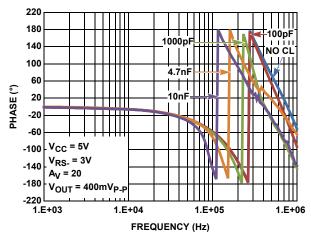


FIGURE 52. CAPACITIVE LOAD DRIVE PHASE VS FREQUENCY

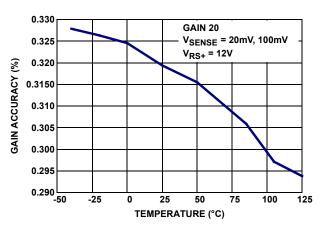


FIGURE 53. GAIN ACCURACY (%) vs TEMPERATURE

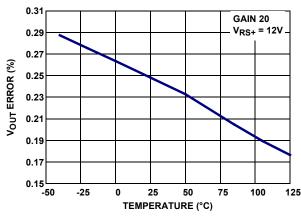


FIGURE 54. V<sub>OUT</sub> ERROR (%) vs TEMPERATURE

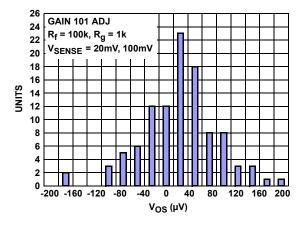


FIGURE 55.  $V_{OS}$  (µV) DISTRIBUTION AT +25 °C,  $V_{RS+}$  = 12V, QUANTITY: 100

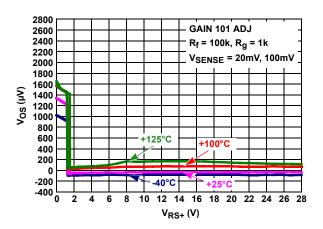


FIGURE 56.  $V_{OS}$  vs  $V_{RS+}$ 

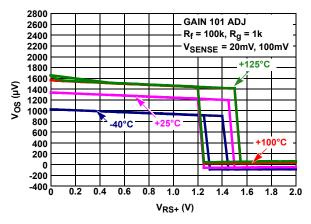


FIGURE 57. VOS vs VRS+

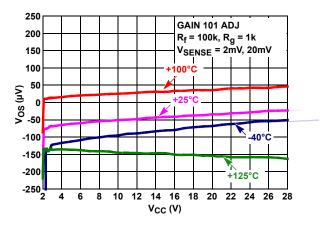


FIGURE 58.  $V_{OS}$  vs  $V_{CC}$ , HIGH-SIDE

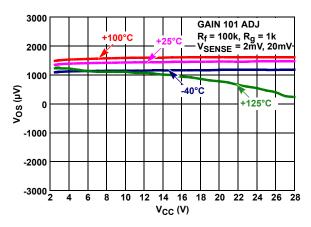


FIGURE 59.  $V_{OS}$  vs  $V_{CC}$ , LOW-SIDE

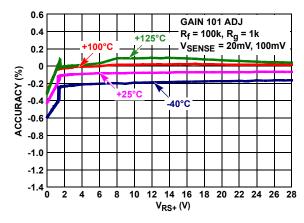


FIGURE 60. GAIN ACCURACY vs  $V_{RS+}$  = 0V TO 28V

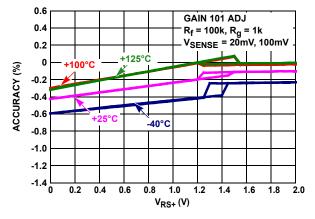


FIGURE 61. GAIN ACCURACY vs V<sub>RS+</sub> = 0V TO 2V

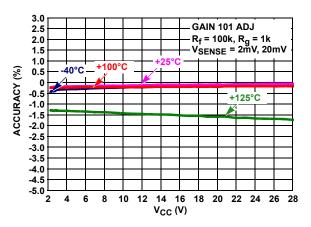


FIGURE 62. GAIN ACCURACY vs V<sub>CC</sub>, V<sub>RS+</sub> = 12V

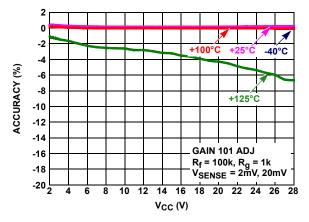


FIGURE 63. GAIN ACCURACY vs V<sub>CC</sub>, V<sub>RS+</sub> = 0.1V

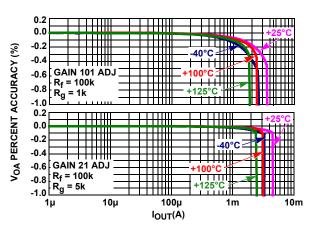


FIGURE 64. NORMALIZED VOA VS IOUT

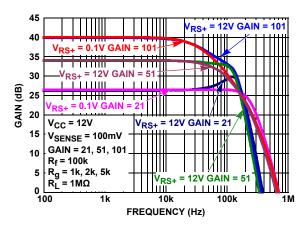


FIGURE 65. GAIN vs FREQUENCY  $V_{RS+} = 100 \text{mV}/12 \text{V},$   $V_{SENSE} = 100 \text{mV}, V_{OUT} = 50 \text{mV}_{P-P}$ 

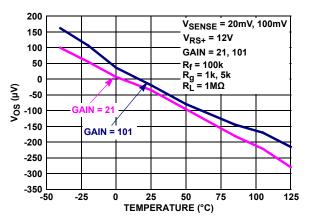


FIGURE 66. V<sub>OS</sub> (μV) vs TEMPERATURE

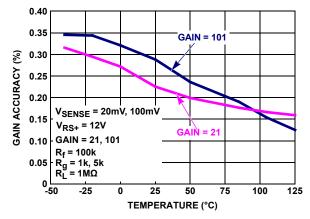


FIGURE 67. GAIN ACCURACY (%) vs TEMPERATURE

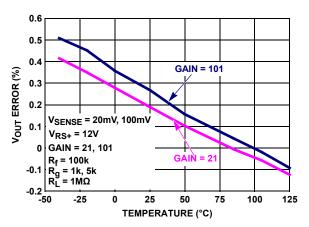


FIGURE 68. V<sub>OUT</sub> ERROR (%) vs TEMPERATURE

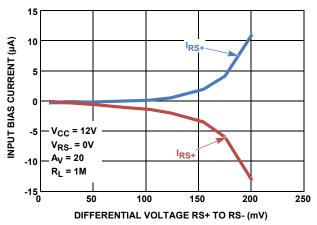


FIGURE 69. LOW SIDE CURRENT SENSING INPUT BIAS CURRENTS

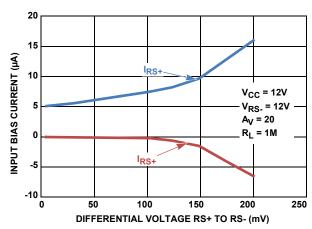


FIGURE 70. HIGH SIDE CURRENT SENSING INPUT BIAS CURRENTS

## **Test Circuits and Waveforms**

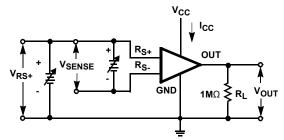


FIGURE 71.  $I_{CC}$ ,  $V_{OS}$ ,  $V_{OA}$ , CMRR, PSRR, GAIN ACCURACY

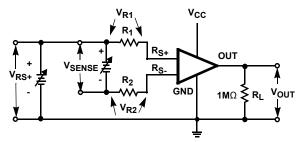


FIGURE 72. INPUT BIAS CURRENT, LEAKAGE CURRENT

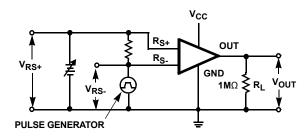


FIGURE 73. t<sub>s</sub>, SATURATION RECOVERY TIME

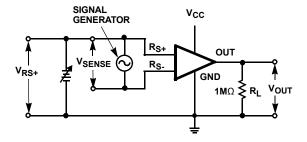


FIGURE 74. GAIN vs FREQUENCY

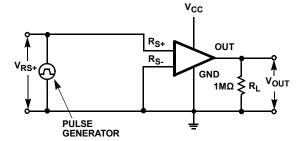


FIGURE 75. SLEW RATE

### **Applications Information**

#### **Functional Description**

The ISL28006-20, ISL28006-50 and ISL28006-100 are single supply, uni-directional current sense amplifiers with fixed gains of 20V/V, 50V/V and 100V/V respectively. The ISL28006-ADJ is single supply, uni-directional current sense amplifier with an adjustable gain via external resistors (see Figure 80). The ISL28006-ADJ is stable for gains of 20 and higher.

The ISL28006 is a 2-stage amplifier. Figure 76 shows the active circuitry for high-side current sense applications where the sense voltage is between 1.35V to 28V. Figure 77 shows the active circuitry for ground sense applications where the sense voltage is between 0V to 1.35V.

The first stage is a bi-level trans-conductance amp and level translator. The gm stage converts the low voltage drop ( $V_{SENSE}$ ) sensed across an external milli-ohm sense resistor, to a current (@ gm = 21.3µA/V). The trans-conductance amplifier forces a current through  $R_1$  resulting to a voltage drop across  $R_1$  that is equal to the sense voltage ( $V_{SENSE}$ ). The current through  $R_1$  is mirrored across  $R_5$  creating a ground-referenced voltage at the input of the second amplifier equal to  $V_{SENSE}$ .

The second stage is responsible for the overall gain and frequency response performance of the device. The fixed gains (20, 50, 100) are set with internal resistors  $R_f$  and  $R_g$ . The variable gain (ADJ) has an additional FB pin and uses external

gain resistors to set the gain of the output. For the fixed gain amps the only external component needed is a current sense resistor (typically  $0.001\Omega$  to  $0.01\Omega$ , 1W to 2W).

The transfer function for the fixed gain parts is given in Equation 1.

$$V_{OUT} = GAIN \times (I_S R_S + V_{OS})$$
 (EQ. 1)

The transfer function for the adjustable gain part is given in Equation 2.

$$\mathbf{V}_{OUT} = \left(\mathbf{1} + \frac{\mathbf{R}_F}{\mathbf{R}_G}\right) (\mathbf{I}_S \mathbf{R}_S + \mathbf{V}_{OS}) \tag{EQ. 2}$$

Where  $I_SR_S$  is the product of the load current and the sense resistor and is equal to  $V_{SENSE}$ .

When the sensed input voltage is >1.35V, the gm $_{HI}$  amplifier path is selected and the input gm stage derives its ~2.86µA supply current from the input source through the RS+ terminal. When the sense voltage at R $_{S}$ + drops below the 1.35V threshold, the gm $_{LO}$  amplifier is enabled for Low Side current sensing. The gm $_{LO}$  input bias current reverses, flowing out of the RS- pin. Since the gm $_{LO}$  amplifier is sensing voltage around ground, it cannot source current to R5. A current mirror referenced off Vcc supplies the current to the second stage for generating a ground referenced output voltage. See Figures 69 and 70 for typical input bias currents for High and Low side current sensing.

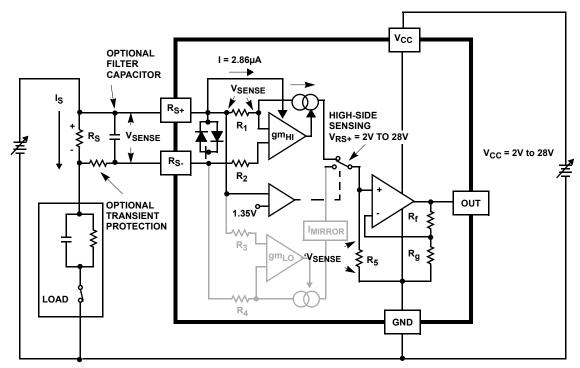


FIGURE 76. HIGH-SIDE CURRENT DETECTION ●

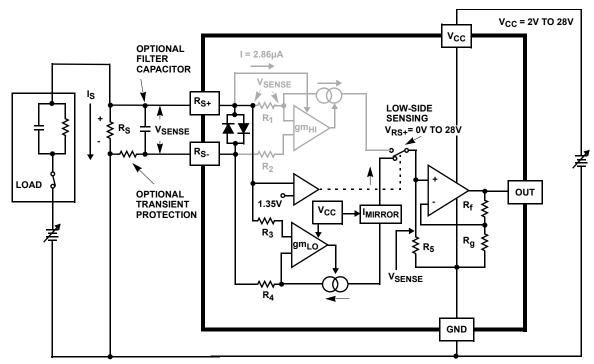


FIGURE 77. LOW-SIDE CURRENT DETECTION

### **Hysteretic Comparator**

The input trans-conductance amps are under control of a hysteretic comparator operating from the incoming source voltage on the  $R_{S+}$  pin (Figure 78). The comparator monitors the voltage on  $R_{S+}$  and switches the sense amplifier from the low-side gm amp to the high-side gm amplifier whenever the input voltage at  $R_{S+}$  increases above the 1.35V threshold. Conversely, a decreasing voltage on the  $R_{S+}$  pin, causes the hysteric comparator to switch from the high-side gm amp to the low-side gm amp as the voltage decreases below 1.35V. It is that low-side sense gm amplifier that gives the ISL28006 the proprietary ability to sense current all the way to 0V. Negative voltages on the  $R_{S+}$  or  $R_{S-}$  are beyond the sensing voltage range of this amplifier.

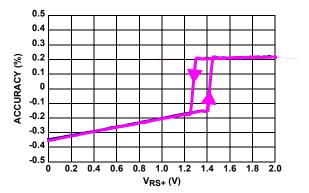


FIGURE 78. GAIN ACCURACY vs V<sub>RS+</sub> = 0V TO 2V

#### **Typical Application Circuit**

Figure 80 shows the basic application circuit and optional protection components for switched-load applications. For applications where the load and the power source is permanently connected, only an external sense resistor is needed. For applications where fast transients are caused by hot plugging the source or load, external protection components may be needed. The external current limiting resistor (Rp) in Figure 80 may be required to limit the peak current through the internal ESD diodes to <20mA. This condition can occur in applications that experience high levels of in-rush current causing high peak voltages that can damage the internal ESD diodes. An Rp resistor

value of  $100\Omega$  will provide protection for a 2V transient with the maximum of 20mA flowing through the input while adding only an additional  $13\mu V$  (worse case over-temperature) of  $V_{OS}$ . Refer to Equation 3:

$$((\textbf{R}_{\textbf{P}}\times\textbf{I}_{\textbf{RS-}})=(\textbf{100}\Omega\times\textbf{130}\,\textbf{nA})=\textbf{13}\,\mu\textbf{V}) \tag{EQ. 3}$$

Switching applications can generate voltage spikes that can overdrive the amplifier input and drive the output of the amplifier into the rails, resulting in a long overload recover time. Capacitors  $\mathbf{C}_{\mathbf{M}}$  and  $\mathbf{C}_{\mathbf{D}}$  filter the common mode and differential voltage spikes.

#### **Error Sources**

There are 3 dominant error sources: gain error, input offset voltage error and Kelvin voltage error (see Figure 79). The gain error is dominated by the internal resistance matching tolerances. The remaining errors appear as sense voltage errors at the input to the amplifier. They are  $\rm V_{OS}$  of the amplifier and Kelvin voltage errors. If the transient protection resistor is added, an additional  $\rm V_{OS}$  error can result from the IxR voltage due to input bias current. The limiting resistor should only be added to the  $\rm R_{S-}$  input, due to the high-side gm amplifier (gm $_{\rm HI}$ ) sinking several micro amps of current through the  $\rm R_{S+}$  pin.

## **Layout Guidelines**

#### **The Kelvin Connected Sense Resistor**

The source of Kelvin voltage errors is illustrated in Figure 79. The resistance of 1/2 Oz copper is ~1m $\Omega$  per square with a TC of ~3900ppm/°C (0.39%/°C). When you compare this unwanted parasitic resistance with the total 1m $\Omega$  to 10m $\Omega$  resistance of the sense resistor, it is easy to see why the sense connection must be chosen very carefully. For example, consider a maximum current of 20A through a 0.005 $\Omega$  sense resistor, generating a V<sub>SENSE</sub> = 0.1 and a full scale output voltage of 10V (G = 100). Two side contacts of only 0.25 square per contact puts the V<sub>SENSE</sub> input about 0.5 x 1m $\Omega$  away from the resistor end capacitor. If only 10A the 20A total current flows through the kelvin path to the resistor, you get an error voltage of 10mV (10A x 0.5sq x 0.001 $\Omega$ /sq. = 10mV) added to the 100mV sense voltage for a sense voltage error of 10% (0.110V-0.1)/0.1V) x 100.

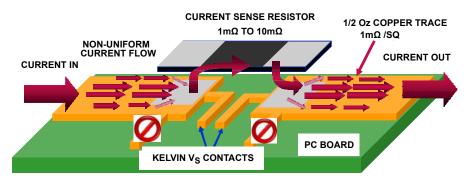


FIGURE 79. PC BOARD CURRENT SENSE KELVIN CONNECTION

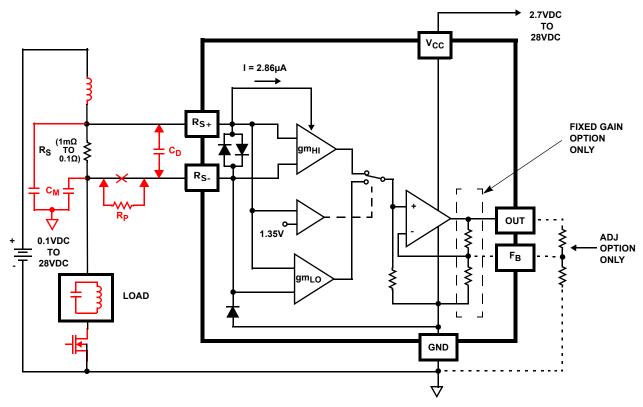


FIGURE 80. TYPICAL APPLICATION CIRCUIT

## Overall Accuracy (VOA %)

 $V_{OA}$  is defined as the total output accuracy Referred-to-Output (RTO). The output accuracy contains all offset and gain errors, at a single output voltage. Equation 4 is used to calculate the % total output accuracy.

$$V_{OA} = 100 \times \left( \frac{V_{OUT} actual - V_{OUT} expected}{V_{OUT} expected} \right)$$
 (EQ. 4)

where

 $V_{OUT}$  Actual =  $V_{SENSE}$  x GAIN

Example: Gain = 100, For 100mV V<sub>SENSE</sub> input we measure 10.1V. The overall accuracy ( $V_{OA}$ ) is 1% as shown in Equation 5.

$$V_{OA} = 100 \times \left(\frac{10.1 - 10}{10}\right) = 1\%$$
 (EQ. 5)

#### **Power Dissipation**

It is possible to exceed the +150°C maximum junction temperatures under certain load and power supply conditions. It is therefore important to calculate the maximum junction temperature (T<sub>JMAX</sub>) for all applications to determine if power supply voltages, load conditions, or package type need to be modified to remain in the safe operating area. These parameters are related using Equation 6:

$$T_{JMAX} = T_{MAX} + \theta_{JA} x PD_{MAXTOTAL}$$
 (EQ. 6)

#### where:

- P<sub>DMAXTOTAL</sub> is the sum of the maximum power dissipation of each amplifier in the package (PDMAX)
- PD<sub>MAX</sub> for each amplifier can be calculated using Equation 7:

$$PD_{MAX} = V_{S} \times I_{qMAX} + (V_{S} - V_{OUTMAX}) \times \frac{V_{OUTMAX}}{R_{I}}$$
 (EQ. 7)

#### where:

- T<sub>MAX</sub> = Maximum ambient temperature
- θ<sub>JA</sub> = Thermal resistance of the package
- PD<sub>MAX</sub> = Maximum power dissipation of 1 amplifier
- V<sub>CC</sub> = Total supply voltage
- I<sub>aMAX</sub> = Maximum quiescent supply current of 1 amplifier
- V<sub>OUTMAX</sub> = Maximum output voltage swing of the application
- R<sub>L</sub> = Load resistance

## **Revision History**

The revision history provided is for informational purposes only and is believed to be accurate, but not warranted. Please go to web to make sure you have the latest Rev.

DATE	REVISION	CHANGE
November 22, 2013	FN6548.6	Added eight new Typical Performance Curves  1. Av=100 Capacitive Load Drive Gain vs Freq  2. Av=100 Capacitive Load Drive Phase vs Freq  3. Av=50 Capacitive Load Drive Gain vs Freq  4. Av=50 Capacitive Load Drive Phase vs Freq  5. Av=20 Capacitive Load Drive Gain vs Freq  6. Av=20 Capacitive Load Drive Phase vs Freq  7. High Side Operation Input Bias Currents  8. Low Side Operation Input Bias Currents  Under Electrical Specifications Table: Changed parameter from Is to Icc to clarify supply current Ordering information table on page 3: Changed Note 4 location in the table.
April 12, 2011	FN6548.5	Converted to new template Page 1 - Changed headings for "Typical Application" and "Gain Accuracy vs VRS+ = 0V to 28V" to Figure titles (Figures 1 and 2). Page 1 - Updated Intersil Trademark statement at bottom of page 1 per directive from Legal. Page 7 - Updated over temp note in Min Max column of spec tables from "Parameters with MIN and/or MAX limits are 100% tested at +25°C, unless otherwise specified. Temperature limits established by characterization and are not production tested." to new standard "Compliance to datasheet limits is assured by one or more methods: production test, characterization and/or design." Page 19 - Figure 69, Low side current detection schematic: Moved the LOAD from the ground side of the power side circuit to the high side.
September 2, 2010	FN6548.4	Added -T7A tape and reel options to Ordering Information Table for all packages.
May 12, 2010	FN6548.3	Added Note 4 to Part Marking Column in "Ordering Information" on page 3. Corrected hyperlinks in Notes 1 and 3 in "Ordering Information" on page 3.
April 8, 2010		Removed "Coming Soon" from evaluation boards in "Ordering Information" on page 3.
April 7, 2010		Added "Related Literature" on page 1 Updated Package Drawing Number in the "Ordering Information" on page 3 for the 20V, 50V and 100V options from MDP0038 to P50.64A. Revised package outline drawing from MDP0038 to P5.064A on page 24. MDP0038 package contained 2 packages for both the 5 and 6 Ld SOT-23. MDP0038 was obsoleted and the packages were separated and made into 2 separate package outline drawings; P5.064A and P6.064A. Changes to the 5 Ld SOT-23 were to move dimensions from table onto drawing, add land pattern and add JEDEC reference number.
March 10, 2010	FN6548.2	Releasing adjustable gain option.  Added adjustable block diagram (Page 2), Added adjustable gain limits to electrical spec table, added Figures 47 through 60, Added +85°C curves to Figures 6 thru 14, 20 thru 28, 34 thru 42, and Figures 48 thru 56. Modified Figure 70.
February 4, 2010	FN6548.1	-Page 1: Edited last sentence of paragraph 2.  Moved order of GAIN listings from 20, 50, 100 to 100, 50, 20 in the 3rd paragraph. Under Featuresremoved "Low Input Offset Voltage 250μV, max" Under Features moved order of parts listing from 20, 50, 100 (from top to bottom) to 100, 50, 20Page 3: Removed coming soon on ISL28006FH50Z and ISL28006FH20Z and changes the order or listing them to 100, 50, 20Page 5: VOA test. Under conditions columndeleted 20mV to. It now reads Vsense = 100mV SR test. Under conditions columndeleted what was there. It now reads Pulse on RS+pin, See Figure 51 -Page 6: ts test. Removed Gain = 100 and Gain = 100V/V in both description and conditions columns respectivelyPage 9: Added VRS+= 12V to Figures 16, 17, 18Page 11: Added VRS+= 12V to Figures 30, 31, 32Page 13 & 14: Added VRS+= 12V to Figures 44, 45, 46Page 14 Added Figure 51 and adjusted figure numbers to account for the added figureFigs 8, 26, and 40 change "HIGH SIDE" to "VRS = 12V", where RS is subscriptFigs 9, 27, and 41 change "LOW SIDE" to "VRS = 0.1V", where RS is subscript.
December 14, 2009	FN6548.0	Initial Release

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### ISL28006

## **About Intersil**

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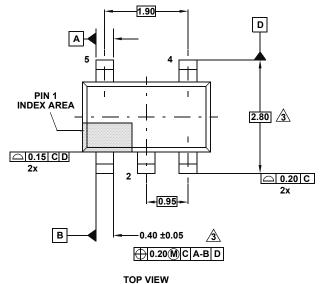
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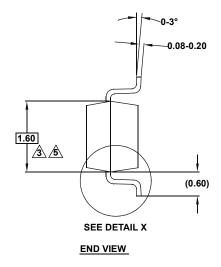
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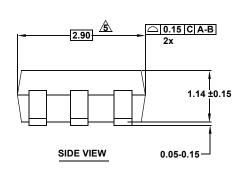
## **Package Outline Drawing**

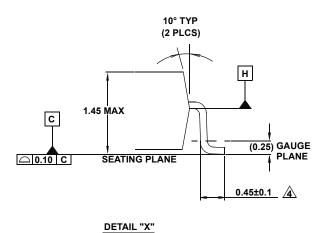
#### P5.064A

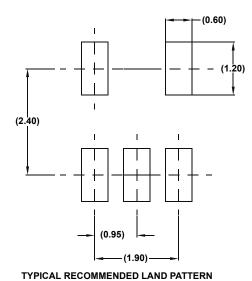
5 LEAD SMALL OUTLINE TRANSISTOR PLASTIC PACKAGE Rev 0, 2/10











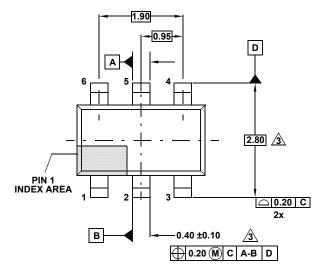
NOTES:

- Dimensions are in millimeters.
   Dimensions in ( ) for Reference Only.
- 2. Dimensioning and tolerancing conform to ASME Y14.5M-1994.
- 3. Dimension is exclusive of mold flash, protrusions or gate burrs.
- 4. Foot length is measured at reference to guage plane.
- 5. This dimension is measured at Datum "H".
- 6. Package conforms to JEDEC MO-178AA.

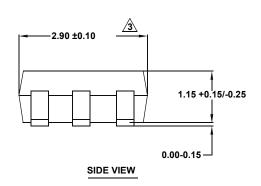
## **Package Outline Drawing**

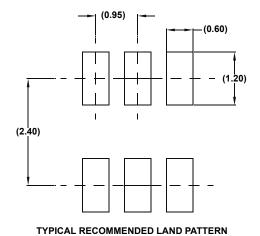
### P6.064

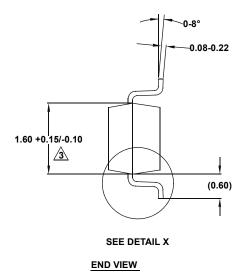
6 LEAD SMALL OUTLINE TRANSISTOR PLASTIC PACKAGE Rev 4, 2/10

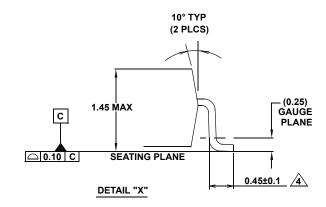


**TOP VIEW** 









#### NOTES:

- Dimensions are in millimeters.
   Dimensions in ( ) for Reference Only.
- 2. Dimensioning and tolerancing conform to ASME Y14.5M-1994.
- 3. Dimension is exclusive of mold flash, protrusions or gate burrs.
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- 5. Package conforms to JEDEC MO-178AB.